

Poster session 6: Concrete structures

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POSTER SESSION 6

Concrete Structures

Structures en béton

Betontragwerke

Coordinator: R.S. Stilwell, Canada



New Column for Tall Reinforced Concrete Buildings

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A twenty-five story condominium constructed by Kajima Corp. is the highest reinforced concrete building in Japan, meeting the structural requirements for earthquake resistance. However, demand for the construction of taller buildings, particularly in urban reconstruction, is increasing. Therefore it has become necessary to develop new structural systems, especially a column system applicable to high-rise buildings taking into account earthquake resistance, economy and execution of works.

Now, in the twenty-five story condominium, the special lateral reinforcement which combines a circular spiral hoop and conventional lateral hoop is used. Since the concrete is effectively restrained by this special lateral reinforcement, it was proved that the restoring force is slightly reduced by cyclic lateral loading as shown in Fig.2.

So, for 30~40 story buildings, we have devised a new column system using high-strength concrete, small-size H-shaped steel and special lateral reinforcements, as shown in Fig.1.

And many specimens were tested to investigate the structural characteristics of the column system. The central compressive force was applied to test specimens as shown in Fig.3. As a result of this test, the maximum load capacity and its reduction ratio for the KS-type column compared to the central compressive force are the same or more than those for the conventional H-type column which uses H-shaped steel with a large sectional area.

The bending and shearing force was applied to test specimens as shown in Fig.4. As a result of these tests, the special lateral reinforcement is superior to the conventional lateral reinforcement on the capacity of restoring force after the maximum load. And the load capacity and ductility of this column are sufficient performance comparing with the conventional column under high compressive or tensile axial load. In addition, this new column has restoring characteristics regardless of the internal H-shaped steel load direction.

As a result of our research, design range of the column has been setting up like Fig.5. And the construction of economical forty-story buildings has been made possible.

NEW COLUMN FOR TALL REINFORCED CONCRETE BUILDINGS

BACKGROUND

In Japan, demand for the construction of 30~40 story condominium is growing. So it has become necessary to develop new column system taking into account earthquake resistance, economy and execution of works.

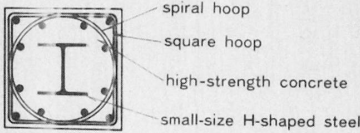


Fig.1 Newly Devised Column

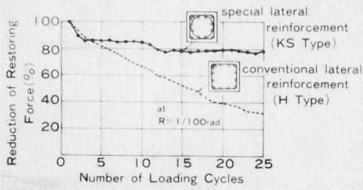


Fig.2 Effects of Special Lateral Reinforcements on Restoring Force for Cyclic Loading

RESEARCH AND DEVELOPMENT

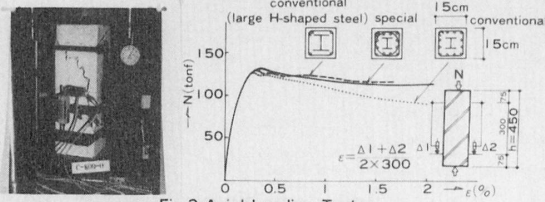


Fig.3 Axial Loading Tests

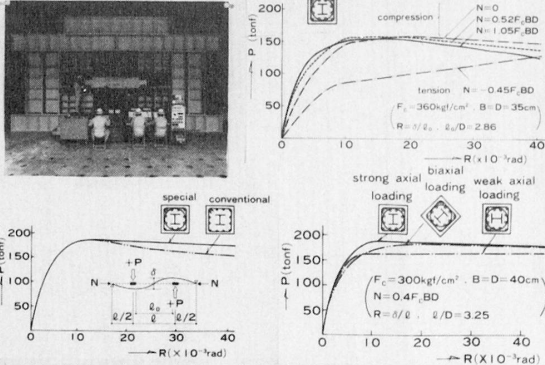


Fig.4 Bending and Shear Tests under Constant Axial Load

DESIGN

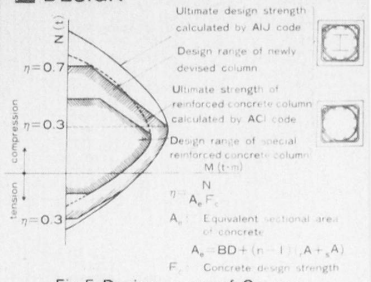


Fig.5 Design Range of Column

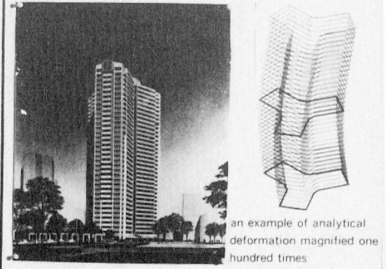


Fig.6 Perspective of First Building in which System to be Applied



Cable Stays for Bridges

H. SCHAMBECK

Civil Eng.

Dyckerhoff & Widmann

München, FR Germany

DYWIDAG POSTTENSIONING SYSTEMS

Type of steel	Steel grade	(mm)	Nominal ultimate load kN							Bell anchorage	OR plate anchorage	Square ribbed plate anchorage	Rectangular rib-bed pl. anchorage	Square solid plate anchorage	Rectangular solid plate anchorage	LO-plate anchorage	Ring plate anchorage	Multi area anchorage	Bond head anchorage	Loop anchorage	Coupler (movable)	Coupler (fixed)	Unbonded tendon
			100	200	400	1000	2000	5000															
Smooth bar	1420/1570	30	●						●												●	●	●
		12,2		●					●												●	●	●
	835/1230	26			●				●												●	●	●
		32				●			●												●	●	●
		36					●		●												●	●	●
	1080/1230	26					●		●												●	●	●
		32						●	●												●	●	●
	36							●	●											●	●	●	
Thread bar	885/1080	15		●					●												●	●	●
	1325/1470	16			●				●												●	●	●
	835/1030	26,5				●			●												●	●	●
		32					●		●												●	●	●
		36						●	●												●	●	●
	1080/1230	26,5					●		●												●	●	●
		32						●	●												●	●	●
	36							●	●											●	●	●	
Strand	1570/1770	10,6			●				●												●	●	●
		3				●			●												●	●	●
		4					●		●												●	●	●
		5						●	●												●	●	●
		7							●												●	●	●
		9								●											●	●	●
		11									●										●	●	●
		12										●									●	●	●
		15											●								●	●	●
		19												●							●	●	●

DYWIDAG CABLES

	Cable type	STRAND CABLE	BAR CABLE
<u>LOAD BEARING</u>			
1 CABLE (Static+Dynamic)		STRAND (7-wire stress-relieved) Grade St 1570/1770 Diameter 0,6" (Low relaxation)	THREADED BARS STEEL TUBES Grade St 835/1030 Grade St 37 Dia. 32, 36 mm (DIN 17 100)
2 ANCHORAGE			
Static		WEDGE ANCHORAGE	NUT ANCHORAGE
Dynamic		Combined WEDGE+BOND ANCHOR	BOND ANCHORAGE
Bending		STEEL TUBES	STEEL TUBES
<u>CORROSION PROTECTION</u>		Multiple anti-corrosion barriers to meet different requirements eg SHEATHING, GROUT, COATING OF STRANDS etc eg STEEL TUBES, GROUT etc	
<u>PRESTRESSING</u>		SINGLE and MULTIPLE STRAND-JACKS	SINGLE BAR-JACKS
<u>CABLE ERECTION</u>		Different procedures to fit into various construction demands eg Erection on site, Prefabrication	
<u>ADDITIONAL FEATURES</u>		FULLY REPLACABLE ADJUSTABLE before and after grouting	REPLACABLE ADJUSTABLE before grouting

CABLE STAYS FOR BRIDGES

CABLE STAYS		EXAMPLES (STRUCTURE AND CONSTRUCTION METHOD)			
<p>TYPICAL CROSS SECTION</p> <p>CONCRETE GRADE B 45- 90 / 65 CM 56 STRANDS TENDONS - 19 4.06 STIRRUP</p> <p>PROTECTIVE CONCR. LAYER WITH ADDIT. REINFORCEMENT IN VEHICLE IMPACT ZONE OF THE CONCRETE STAY</p> <p>CONSTRUCTION ON SCAFFOLDING WITH POST-TENSIONED PRESTRESSING</p> <p>STRUCTURAL CRITERIA</p> <p>THE CONCR. STAY IS DESIGNED AS BEAM WITH FIXED ENDS STRESSED BY AXIAL TENSION FORCE AND STRESSED BY BENDING MOMENTS DUE TO DEAD WEIGHT OF STAY AND DUE TO WIND LOAD.</p> <p>CHECK OF STRESSES FOR PRESTR. CONCRETE MEMBERS ACC. TO GERMAN CODE DIN 4227</p> <p>CHARACTERISTICS</p> <p>ALLOW TENS. FORCE/SQM OF CONCR. STAY 45-55 MN UNIFORM PRESTR. CONCR. DESIGN FOR TOTAL STRUCTURE INCL. STAY AND ANCHOR BLOCK.</p> <p>STRUCTURE WITH SMALL DEFLECTIONS</p> <p>PERFECT PROTECTION AGAINST CORROSION</p> <p>RELIABLE RESISTANCE AGAINST VEHICLE IMPACT AND SIMILAR DAMAGES</p> <p>NO MAINTENANCE</p> <p>POSSIBILITIES FOR INDIVID. ARCHITECT. DESIGN</p> <p>1/4" OF GIRDER SPAN AT 250 M APPROX. DUE TO DEAD WEIGHT OF CONCRETE STAY</p>	<p>DANUBE RIVER BRIDGE, METTEN, FRG.</p> <p>ELEVATION</p> <p>DETAIL C'</p> <p>DETAIL D'</p> <p>CONSTRUCTION STAGES</p> <p>INCREMENTAL LAUNCHING</p> <p>CASTING OF STAY ON SCAFFOLDING</p>	<p>FLOSSER BRIDGE, FRANKFURT/M, FRG.</p> <p>ELEVATION</p> <p>DETAIL A</p> <p>B-B</p> <p>C-C</p> <p>FREE CANTILEVER WITH TEMPORARY STEEL CABLES</p> <p>CASTING OF STAY ON SCAFFOLDING</p> <p>ARRANGEMENT OF FREE CANTILEVER SEGMENTS</p>	<p>DESIGN WITH CABLE STAYS ARRANGED BELOW GIRDER</p> <p>ELEVATION</p> <p>DETAIL A</p> <p>B-B</p> <p>C-C</p>		
	<p>COMPOSITE CROSS SECTION</p> <p>WIRE ST 125/1470, DIA. 16 MM (W) + STEEL TUBE (ST)</p> <p>FIXED END</p> <p>STEEL TUBE WITH INCREASED WALL THICKNESS</p> <p>LOAD TRANSFER AT ANCHORAGE</p> <p>DEAD LOAD VIA THREADS OF WIRE (T) FATIGUE LOADS VIA BOND ANCHORAGE ZONE II</p>	<p>MAIN RIVER BRIDGE, HOECHST AG, FRG.</p> <p>ELEVATION</p> <p>ANCHORAGE IN TOWER</p> <p>IN GRIDER</p> <p>TOP VIEW</p> <p>SIMULTANEOUS SEGMENTAL CONSTRUCTION</p>	<p>COMPOSITE CROSS SECTION</p> <p>WIRE ST 932/1279, DIA. 32 & 36 MM (B) + STEEL TUBE (ST)</p> <p>FIXED END</p> <p>STEEL TUBE</p> <p>LOAD TRANSFER AT ANCHORAGE</p> <p>DEAD LOAD VIA THREADS OF BARS (T) FATIGUE LOADS VIA BOND ANCHORAGE ZONE II</p>	<p>PENANG BRIDGE, MALAYSIA</p> <p>ELEVATION</p> <p>ANCHORAGE IN TOWER</p> <p>IN GRIDER</p> <p>TOP VIEW</p> <p>SEGMENTAL CONSTRUCTION</p>	
	<p>COMPOSITE CROSS SECTION</p> <p>STRANDS ST 1560/1860, DIA. 0.6" (S)</p> <p>FIXED END</p> <p>ANCHOR STEEL TUBE</p> <p>LOAD TRANSFER AT ANCHORAGE</p> <p>DEAD LOAD VIA WEDGES OF STRANDS (T) FATIGUE LOADS VIA BOND ANCHORAGE ZONE II</p>	<p>FA ROUTE 63 OVER MISSISSIPPI RIVER, QUINCY, ILLINOIS, U.S.A.</p> <p>ELEVATION</p> <p>ANCHORAGE IN TOWER</p> <p>CONSTR. STAGES</p> <p>IN GRIDER</p>	<p>CONSTRUCTION STAGES</p> <p>CASTING OF STAY ON SCAFFOLDING</p> <p>ARRANGEMENT OF FREE CANTILEVER SEGMENTS</p>	<p>CONSTRUCTION STAGES</p> <p>INCREMENTAL LAUNCHING</p> <p>CASTING OF STAY ON SCAFFOLDING</p> <p>ARRANGEMENT OF FREE CANTILEVER SEGMENTS</p>	



Rehabilitation of Post-Tensioned Bridge Deck

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Cowiconsult

Virum, Denmark

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Chief Bridge Eng.
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Virum, Denmark

The bridge was constructed in 1967 and hereafter regular routine inspections were carried out. In 1981 a major examination took place. Larger zones of deteriorated concrete were found in one of the cantilevered flanges, especially in areas near the abutments.

The bridge deck surface has a cross slope of 6% and consequently damage had only taken place in the lower cantilever, and fortunately not in the central part of the girder where the longitudinal main tendons are positioned. This distribution of the damage made repair possible. A full replacement of the superstructure would have resulted in an expenditure of more than 250% of the repair cost and almost total closure of one of the major motorways in Denmark.

The deterioration had started due to a leak in the waterproofing membrane. Unfortunately, the underneath concrete was not resistant against alkaline reactions.

- * - * - * - * - * -

After removal of the bridge deck pavement and water proofing, the deteriorated areas were surveyed by core drilling.

The deteriorated concrete was removed, however, in such a way that the reinforcement and prestressing tendons were not harmed. In this context it was very important that the transverse prestressing in the cantilevers could be reestablished. The transverse prestressing tendons consist of 12 dia. 5 mm wires. In order to protect these wires, the original sheath and grout were not removed until just before the new sheathing was ready to be installed. As it can be seen from the original transverse tendon arrangement, it was not possible to reuse the existing anchorages.

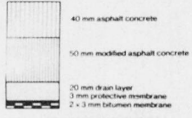
A new system was developed by Skandinavisk Spændbeton. A simple bar anchorage with thread and nut was connected to the wires. The details are shown on the poster. After casting the deck the wires were re-stressed and grouted.

Due to the repair work the longitudinal prestressing forces were lost in the cantilever. Consequently, it was necessary to place some additional ordinary reinforcement in the longitudinal direction, especially at the end of the bridge deck.

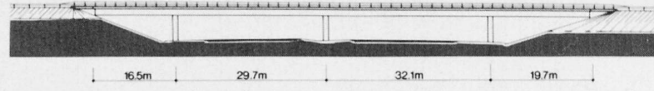
REHABILITATION OF POST-TENSIONED BRIDGE DECK

Bridge data

Year of construction: 1967
 Year of repair: 1982
 Post-tensioned concrete superstructure.
 Ultimate cylinder strength, $f_{ck} \geq 45 \text{ MPa}$
 Longitudinal prestressing
 12 x 0.5 strands, grade 160/180
 Transverse prestressing
 12 x 5 mm wires, grade 150/170
 System Freyssinet
 New waterproofing and pavement:



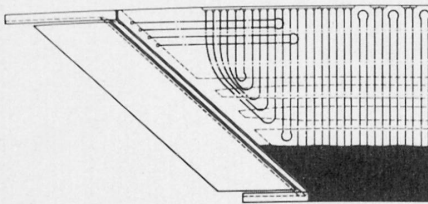
Motorway Bridge, Denmark



Plan

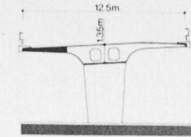


Plan section



Existing transverse and longitudinal prestressing. The 12 x 5 mm transverse prestressing wires were re-used, but cut off at the edge of the bridge deck.

Cross section



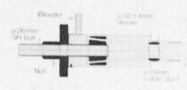
Cantilever section



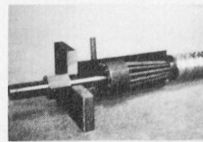
After cut-off, the 12 x 5 mm bars were prepared for coupling with simple bar anchorages. The 5 mm bars were provided with button heads on site.



Re-established transverse prestressing



Coupler and anchorage principle. (System developed by Skandinavisk Spændbeton).



Section through coupler and anchorage.



Wind Structure Interaction on 235 m Tall RCC TV Tower in Delhi

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Bangalore University
Bangalore, India

All India Radio has started the construction of an RCC TV tower, the first of its kind in India, 235 M height with revolving restaurant and viewing gallery at top, in the North - West suburban parts of Delhi, surrounded by industrial and residential area.

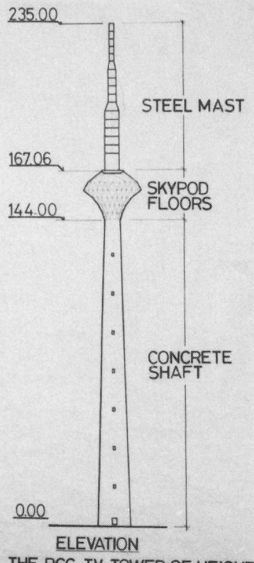
In connection with the above design Indian Meteorological Department (IMD) was requested to undertake analysis of surface and pilot balloon winds at Delhi air-port, to obtain wind escalation law. Utilising available surface upper wind and temperature data spread over long periods, IMD obtained the extreme values of wind and return period with different confidence limits. IMD further correlated the IS code wind figures with the extreme values obtained by their study, indicating the probabilities of occurrence of tornado and storms with return period, by determining maximum wind causing collapse of the structure.

The highest wind value recorded was 159 km/h in 1960. Wind speed for return period 100 years was determined at 175 km/h. For this, with confidence level (95%) and correction (31) wind speed was obtained as 206 km/h for the design. Since Delhi was affected by severetornado in 1978 with damaging wind speed of 250 km/h, the value of the power law co-efficient was worked out to be $1/9$ under unstable and neutral conditions and $1/3$ for stable conditions.

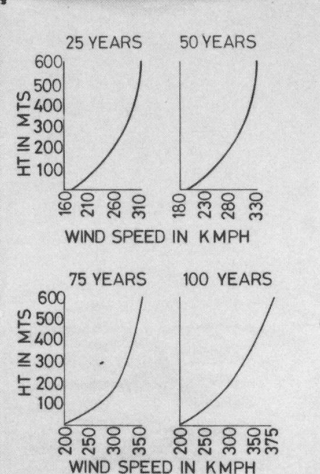
The power-law co-efficient $1/7$ suitable for the change of gust speed with height was used for deriving wind profile.

Wind profile and a few structural details of pile cap, shaft and mast of this unique tower are shown in the photograph.

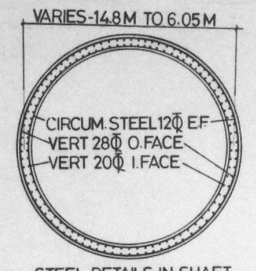
WIND STRUCTURE INTERACTION ON 235 M TALL RCC TV TOWER



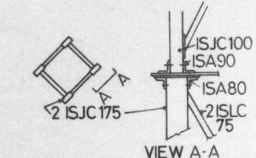
ELEVATION
 THE RCC TV TOWER OF HEIGHT 235M TS. IS THE FIRST OF ITS KIND IN INDIA WITH REVOLVING RESTAURANT AND VIEWING GALLERY AT TOP. THE TOWER IS COMING UP IN NEW DELHI.



WIND PROFILE IN THE REGION OF DELHI BASED ON CONFIDENCE LIMIT 95%. FOR THE HIGHEST WIND SPEED AT SURFACE WITH RETURN PERIOD 100 YEARS WAS DETERMINED AT 175 KM/H. FOR THIS WITH CONFIDENCE LEVEL 95% AND CORRECTION 31 WIND SPEED WAS OBTAINED AS 206 KM/H FOR DESIGN.



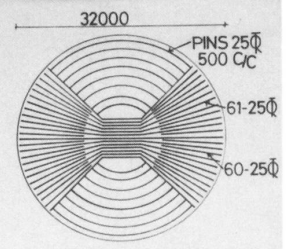
STEEL DETAILS IN SHAFT



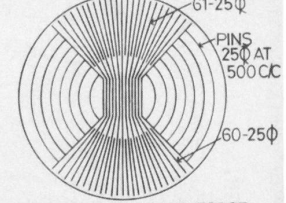
VIEW A-A

TYP DETAIL OF JOINT-MAST
 WIND VELOCITY 162 KM/H AT 10M HT. POWER LAW INDEX 1/κ - 1/7. GUST FACTOR 1.35; DRAG CO-EFF OF 1.1 FOR MAST & SKYPOD AND 0.7 FOR SHAFT IS CONSIDERED FOR DESIGN.

SKYPOD IS DESIGNED AS COMPOSITE SECTION WHICH IS A COMBINATION OF STRUCTURAL STEEL AND REINFORCED CONCRETE.



PLAN DETAILS OF REINFORCEMENT FOR 1, 4, 7, 10 & 13TH LAYER AT BOTTOM AND 16TH LAYER AT TOP. CONCRETE MIX M 250. THERE ARE TOTALLY 15 LAYERS AT BOTTOM AND 3 LAYERS AT TOP.



PLAN DETAILS OF REINFORCEMENT FOR LAYERS 2, 5, 8, 11 & 14 AT BOTTOM AND LAYER 17 AT TOP. ALL OTHER LAYERS ARE TANGENTIAL BARS. PINS OF LAYER 1 ARE BENT UP TO FORM PINS OF LAYER 2 AND HENCE CONTINUOUS.



Continuous Reinforced Concrete Pavement on Bridges

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Continuous reinforced concrete pavement is widely used in Belgium since 1970. It consists of a 20 cm thick slab lying on an adequate foundation.

The longer the segments are, without transversal joints, the better. It is therefore very useful to pass over the under bridges and to avoid expansion joints.

The problem is important in Belgium because of the high density of the highway network and the short intervals between bridges.

Small frame bridges (10-20 m span) can be overpassed without problem.

More complex is the case of bridges with precast girders, the pavement lying on the deck slab with a friction interface.

The last evolution is to use the pavement as bridge slab, supported on the superstructure frame by "neopreen" bearings. Steel beams are incorporated in the pavement.

The main problems are :

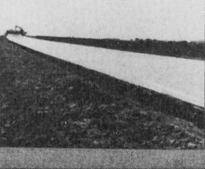
- behaviour of the pavement between the embankments, behind the abutments, and the bridge (differential settling)
- interaction between pavement and bridge deck (deflection, expansion)

1400 Km continuous reinforced concrete pavement (2 ways) are in service in Belgium. The longest bridge overpassed is 136 m long and the greatest span is 65 m long.

CONTINUOUS REINFORCED CONCRETE PAVEMENT ON BRIDGES

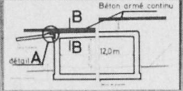
I Revêtement routier en béton armé continu

béton armé 0,20m
 armure hydrocarboné 0,25m
 béton magre 0,20m
 matériau drainant

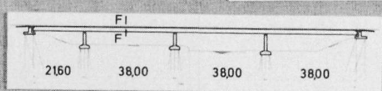
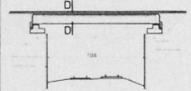


II Le franchissement des ponts

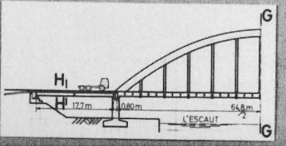
Ponts inférieurs rigides et massifs



Ponts à poutres et dalle



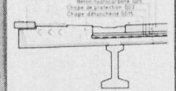
Ponts de grande portée



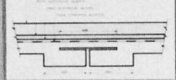
Coupe B-B



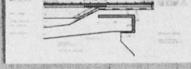
Coupe D-D



Détail E



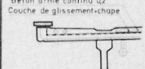
Détail A



Détail E



Coupe F-F



Détail I

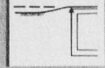


Coupe H-H

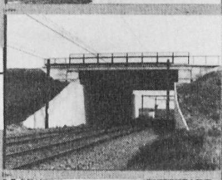
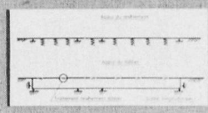


III Particularités, problèmes

Transition remblai-tablier



Interaction revêtement-tablier



Saudi Arabia – Bahrain Causeway

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General

The Causeway incorporates 5 bridges and 7 embankments. The superstructure of the bridges consists of 2 separate boxgirders, each 12,3 m wide, prestressed in both longitudinal and transverse direction.

The bridges have a spanlength of 50 m and are constructed as a "Gerber" structure: alternatively cantilever girders of 66 m and drop in spans (suspende girders) of 34 m. Both cantilever and suspended girders have been prefabricated on shore and are placed in position as a complete unit.

The substructure consists of prefabricated hollow prestressed piles with an outer diameter of 3,5 m. Bridge no. 5 has been founded on caissons due to the presence of an aquifer. Bridge no. 3 incorporates the main navigation span. This navigation span has been constructed in accordance with the prefabricated segmental system.

Spanlengths: 80-150-80 m. The cast in situ piers rest on direct foundations.

Durability

Special measures have been taken because of the very aggressive environment:

- Blast furnace Portland cement (slag content 70-80%) has been used. This cement has a high sulphate resistance and a high impermeability.
- A max Cl^- ion content of 0,1% by weight of cement has been prescribed for the concrete. As a result the sand, dredged from the sea, had to be washed extensively.
- Cover to the rebar for the piles 70 mm, for the superstructure 50 mm.
- The piles have been epoxy coated from -2,0 CD to +4,0 CD (splash zone).

Design criteria

In accordance with AASHTO, with some exceptions regarding the loading:

- lane loads : 10 kN/m' lane.
- trucks : 2 trucks, one of 600 kN and one of 300 kN.
- future pipeline : 10 kN/m', situated 4,5 m outside centre line of bridge
- earthquake : static load consisting of 6% of the permanent vertical load.
- ship collision : -56000 kN on each of the two mainspan piers.
-28000 kN on each of the side piers of the mainspan.
-varying load of 300-1000 kN for the piers adjacent to navigation spans.

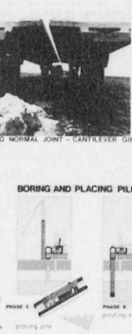
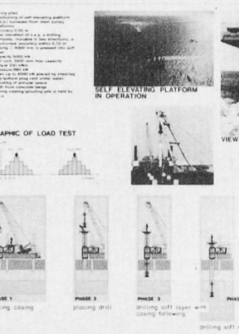
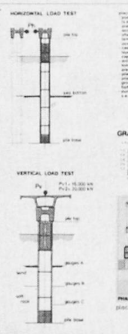
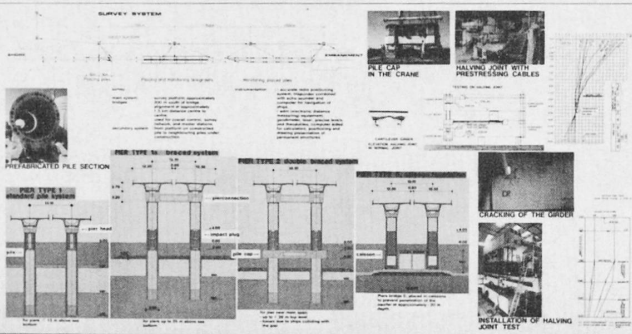
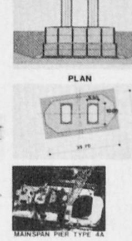
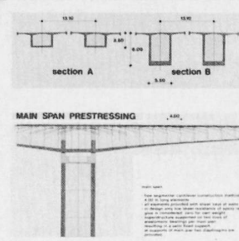
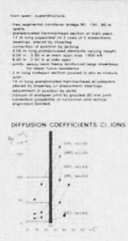
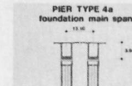
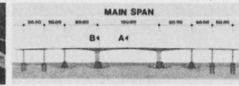
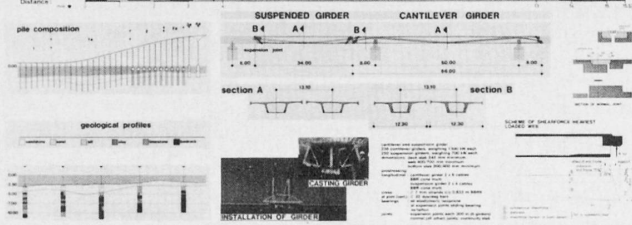
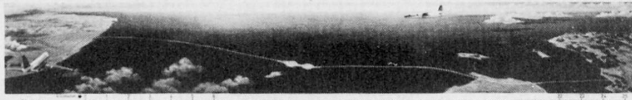
Materials

- Concrete quality : $f_c = 40 \text{ N/mm}^2$ for prefabricated part of halving joint.
 $f_c = 35 \text{ N/mm}^2$ for all structural elements.
- Reinforcement steel : Fe B 400 and Fe B 500 ($f_y = 400 \text{ N/mm}^2$ and 500 N/mm^2 respectively)
- Prestressing steel : Longitudinal prestressing, consisting of BBR CONA-MULTI 0,62" strands: $f_{pu} = 1770 \text{ N/mm}^2$.
Transverse prestressing, consisting of BBRV 7 mm wires: $f_{pu} = 1670 \text{ N/mm}^2$.
Inclined Dywidag bars in halving joints $f_{pu} = 1035 \text{ N/mm}^2$

Soil conditions

- sea bottom 4.00 to 12.00 minus CD.
- top layer of caprock 0.00 - 3.00 m thick.
- soft soil (sand/clay) 2.00 - 8.00 m thick.
- soft rock of claystone/siltstone.

SAUDI ARABIA-BAHRAIN CAUSEWAY

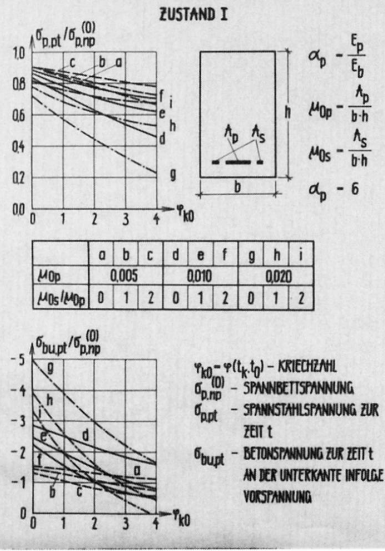


300 metres bridge per week

8 piles drilled and placed every week

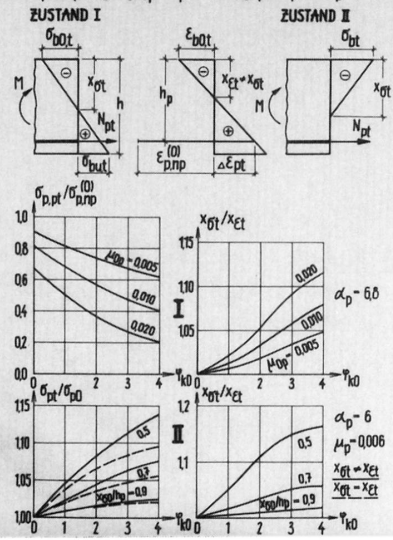
WIRKLICHKEITSNAHE ERFASSUNG DES BETONLANGZEITVERHALTENS

EINFLUSS DER SCHLAFEN BEWEHRUNG (A_s) AUF DIE SPANNUNGSUMLAGERUNGEN

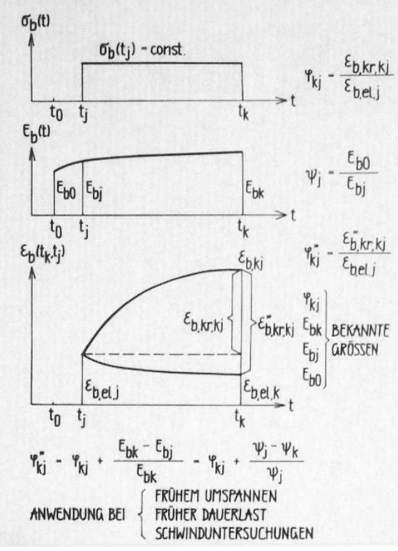


DRUCKZONENHÖHE x_{St} , STAUCHUNGSZONENHÖHE x_{Et} , SPANNSTRESSSPANNUNGEN σ_{pt}

$\alpha_p = E_p/E_b$; $\mu_{Op} = A_p/(b \cdot h)$; $\mu_p = A_p/(b \cdot h_p)$



BERÜCKSICHTIGUNG DER ZEITABHÄNGIGKEIT DES E_b -MODULS



ANALYSIS OF CONCRETE PIER WITH ASEISMATIC WALL

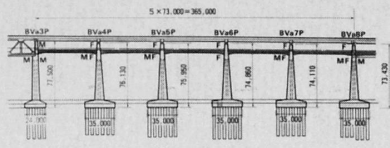


Fig-1 General view of Bannosu Viaduct

1. Bannosu viaduct, the highway-railway combined bridge, has high-rise piers with piles of 3 m in diameter.

Elasto-plastic FEM analysis and loading experiment with a 1/10 model were carried out to evaluate and to estimate the ultimate bearing capacity of concrete pier with aseismatic wall as well as the horizontal displacement at the rail level.

The cases of analysis by FEM consist of four cases as shown in Table-1

The model for analysis is two dimensional and composed of concrete elements, reinforced ones, and bond ones to link both.

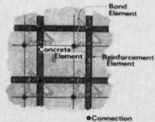


Fig-3 FEM Element

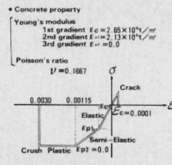


Fig-4 Concrete stress vs strain

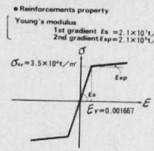


Fig-5 Reinforcements stress vs strain

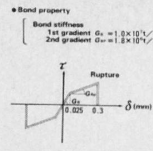


Fig-6 Bond stress vs displacement

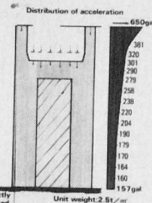
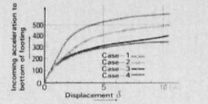
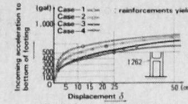


Fig-7 Distribution of load

2. Consideration

As shown in Fig-8, the pier does not show sudden deformation and can keep its shape at the time of cracks generation or reinforcements yielding. This is also confirmed by the experiment with a 1/10 model. The ultimate bearing capacity of the lower column is judged to be more than 3.5 times the design load.

| Case No. | Results strength of concrete | Rate of concrete strength | Purpose of analysis |
|----------|--|---------------------------|---|
| Case-1 | Considered on $\sigma_c = 2.85 \times 10^4 \text{ N/cm}^2$ or $\sigma_c = 2.13 \times 10^4 \text{ N/cm}^2$ | 0.5 | Basic case |
| Case-2 | Considered on $\sigma_c = 2.85 \times 10^4 \text{ N/cm}^2$ or $\sigma_c = 2.13 \times 10^4 \text{ N/cm}^2$ | 0.5 | Influence of initial deterioration of wall due to shrinkage |
| Case-3 | Ignored for both | 0.5 | Influence of initial deterioration of pier due to earthquake aging factor |
| Case-4 | Ignored for both | 0.5 | Influence of rate of reinforcement as well as case-3 |



Followings show progress of concrete cracking (Case-1)

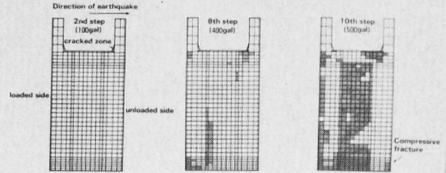
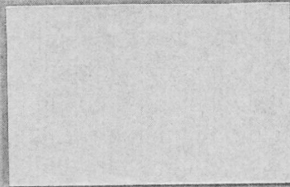


Fig-10 Progress of destruction (Case-1)

PONTS DU ROI TAKSIN-BANGKOK, THAILAND



CARACTERISTIQUES DES OUVRAGES

OUVRAGE EN RIVIERE

Deux tabliers parallèles = longueur 224.00 m

= largeur 13.25 m

Portées 66.00 m - 92.00 m - 66.00 m

VIADUCS D'ACCES

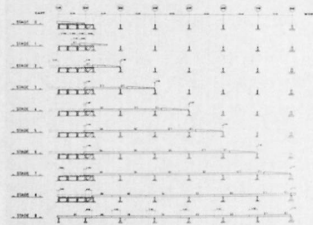
4 ouvrages = longueur 385.00 m

= largeur 11.51 m

Portées courantes = 45.00 m

VIADUCS D'ACCES

PHASES DE POUSAGE



OUVRAGE EN RIVIERE

