

# Composite steel-concrete components: current state of the art and future possibilities

Autor(en): **Klingsch, W. / Schleich, J.B.**

Objektyp: **Article**

Zeitschrift: **IABSE reports = Rapports AIPC = IVBH Berichte**

Band (Jahr): **48 (1985)**

PDF erstellt am: **17.09.2024**

Persistenter Link: <https://doi.org/10.5169/seals-37464>

## **Nutzungsbedingungen**

Die ETH-Bibliothek ist Anbieterin der digitalisierten Zeitschriften. Sie besitzt keine Urheberrechte an den Inhalten der Zeitschriften. Die Rechte liegen in der Regel bei den Herausgebern.

Die auf der Plattform e-periodica veröffentlichten Dokumente stehen für nicht-kommerzielle Zwecke in Lehre und Forschung sowie für die private Nutzung frei zur Verfügung. Einzelne Dateien oder Ausdrucke aus diesem Angebot können zusammen mit diesen Nutzungsbedingungen und den korrekten Herkunftsbezeichnungen weitergegeben werden.

Das Veröffentlichen von Bildern in Print- und Online-Publikationen ist nur mit vorheriger Genehmigung der Rechteinhaber erlaubt. Die systematische Speicherung von Teilen des elektronischen Angebots auf anderen Servern bedarf ebenfalls des schriftlichen Einverständnisses der Rechteinhaber.

## **Haftungsausschluss**

Alle Angaben erfolgen ohne Gewähr für Vollständigkeit oder Richtigkeit. Es wird keine Haftung übernommen für Schäden durch die Verwendung von Informationen aus diesem Online-Angebot oder durch das Fehlen von Informationen. Dies gilt auch für Inhalte Dritter, die über dieses Angebot zugänglich sind.

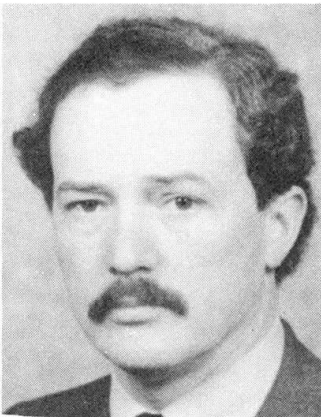
## Composite Steel-Concrete Components: Current State of the Art and Future Possibilities

Eléments structuraux mixtes acier-béton: progrès récents et futurs

Stahl-Beton Verbundteile: gegenwärtige Erkenntnisse und Zukunftsaussichten

### W. KLINGSCH

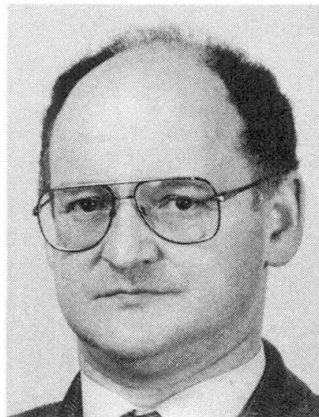
Prof. Dr. Ing.  
University Wuppertal  
Wuppertal, Fed. Rep. Germany



Wolfram Klingsch, born 1944, Dipl.-Ing. degree in 1970, doctor's degree in 1975. Activities as scientist, lecturer and consulting engineer. Since 1982 he holds the chair of building materials technology and fire safety at Bergische University Wuppertal; director of material testing station and institute of constructional engineering.

### J. B. SCHLEICH

Department Manager  
ARBED-Recherches  
Luxembourg



J.B. Schleich, born 1942, got his civil engineering degree at the Univ. of Liège, where he was involved for two years in teaching and research. He then got active for eleven years in the constructional steelwork industry in Luxembourg. He is now responsible for the research on steel construction at ARBED's Research Centre, Luxembourg. President of the ECCS in 1985.

### SUMMARY

The paper gives a survey of the most commonly used composite cross-section types, deals with architectural and practical points of view, and shows the future possibilities of the newly developed thermo-mechanical numerical computer codes and of new material technologies.

### RÉSUMÉ

Cette contribution donne un aperçu sur les sections mixtes les plus usuelles, traite de points de vue d'architecture et de la pratique, et indique les perspectives d'avenir concernant les nouveaux programmes de calcul thermo-mécaniques et numériques ainsi que les nouvelles technologies à venir dans le domaine des matériaux.

### ZUSAMMENFASSUNG

Dieser Text gibt eine Übersicht von den gebräuchlichsten Verbundquerschnitten, behandelt architektonische und praktische Gesichtspunkte, und beleuchtet zusätzlich die Zukunftsaussichten der neuen thermo-mechanischen, numerischen DV-Programme sowie der neu zu erwartenden Materialtechnologien.

## 1. Introduction

The base principle of composite steel-concrete constructions consists in combining ideally advantageous characteristics of both materials steel and concrete. Ductility, high-tension-strength and easy prefabrication are procured by the steel component; high compressive strength and low thermal diffusibility ( $\lambda/c, \rho$ ) are supplied by the concrete component. In a composite cross section these single parameters don't just add, but activate new additional effects like high stiffness for slender members, high rotation capacity, higher load bearing capacity etc. Therefore composite steel-concrete structural elements are coming into favour for all typical building applications.

The possibility of using visible steel as load bearing component, even for fire resistant structural elements, opens new and trendsetting aspects for architectural design concepts (fig. 1).

## 2. Present time acuirements

### 2.1. Slabs

Steel-concrete composite slabs are commonly based on a cold rolled profiled steel sheet supporting the concrete deck. Using special shaped steel sheets, no additional reinforcement is required as well for normal temperature load bearing capacity as under fire load [1]. Quick and easy setting up of such slabs, due to concreting without additional supports, to easy beam connections and to a steel sheet surface ready for use allow very economic applications.

### 2.2. Beams

Hot rolled steel profiles acting as shear connected beams with a concrete or a composite slab are well known structural elements. High load bearing capacity, high bending stiffness, easy prefabrication and a practically always given feasibility explain why this type of composite element is nowadays so largely involved in the field of industrial and office buildings.

A new technology [2,3] for fireproof elements allows to do definitively without cladding of the steel surfaces by concreting between the profile flanges (fig. 2). The lower flange remains as an unprotected visible steel surface. In industrial buildings this is of the highest advantage for making connections by welding at any time not only during the construction procedure but also later for constructional modifications.

Concrete filled beams of this type, but without shear connections to the concrete plate reach higher load bearing capacity than simple steel beams by activating the concrete filling in the compression zone. The same advantage exists for this type of composite beam when used as cantilever, where negative bending moments become the predominant load effect. For fire design the proportional loss of load bearing capacity from the unprotected steel flange, must be compensated by reinforcing bars (fig. 3) or steel strips welded to the web.

These numerous advantages undoubtedly are leading to a dominating application of this type of composite beams in case of fire resistance requirements.

### 2.3. Columns

Three basic types of cross-section design (fig. 4, 5, 6) lead to the standard steel-concrete composite columns:

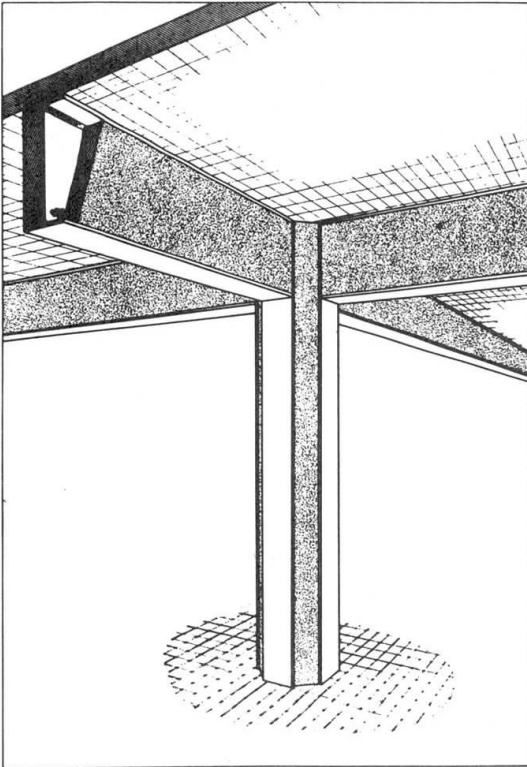


Fig. 1 Octagonal composite column supporting four composite beams, high fire resistance and visible steel

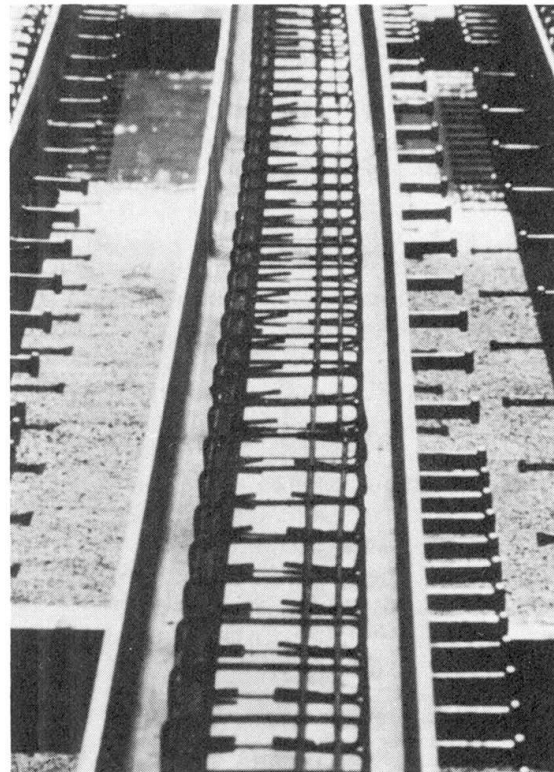


Fig. 2 AF 90 beams before concreting: Office building Magnus Müller, Delmenhorst W-Germany, 1982

Fig. 3 Design diagram for AF composite beams [7] using HE-AA profiles of ARBED ( $\beta_y/\beta_c = 355/35 \text{ N/mm}^2$ ). (Hatched part:  $f_{q,0} \leq L/300$  at ambient temperature

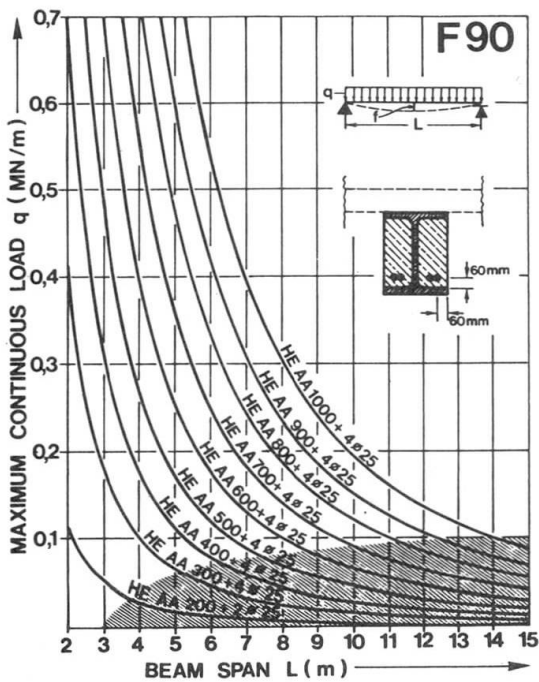
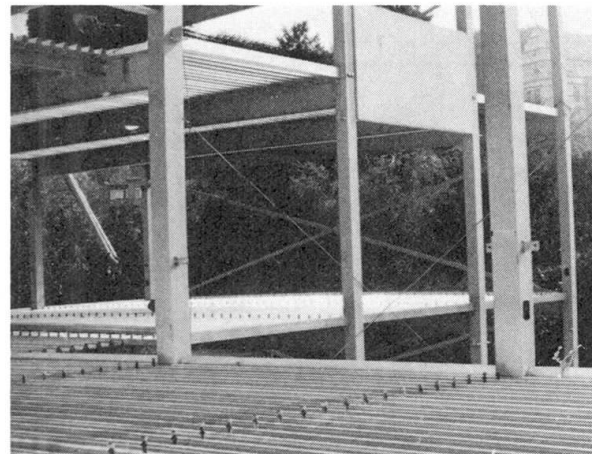


Fig. 4 Hollow section composite columns (openings for concrete filling): Office building, Bielefeld, W-Germany, 1980



- hollow sections filled with concrete [4],
- hot rolled profiles concreted between the flanges [2,3],
- hot rolled profiles completely encased in concrete [5].

Under normal temperature conditions load bearing behaviour and hence design procedures are uniform for all these types of composite columns. But every type has different fire behaviour characteristics. The reason is the different location and consequently the different heating behaviour of the steel component. Columns with higher percentage of unprotected steel, show reduction in load bearing capacity sooner than those with steel completely protected by the concrete component.

For fire design the uniform service load calculation concept must be modified and adapted to each different cross section type.

All the mentioned column types can be designed for high fire resistance times [6]. The key for this, is the realistic consideration of the internal interaction between the cross section components. A credible fire design therefore must be based on numerical methods. Service load tables for normal temperature conditions and ultimate load tables attached to fire resistance classes have been calculated in this way (fig. 7,8,9).

#### 2.4. Structures

The creation of complete steel-concrete composite structures indicates a new tendency in building technology, especially in industrial and office buildings. The advantages are numerous: prefabrication, easy fitting (fig. 10), reduced erection time and hence, lower financial costs.

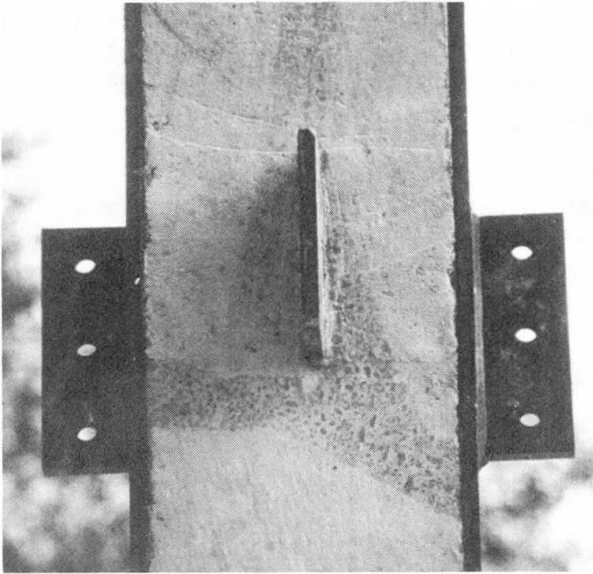
In fire design the step from the single member calculation to the global structural analysis should activate additional economic advantages for instance given by the frame stiffening of columns or the bending moment rearrangement possible with continuous beams. Two options are offered: higher fire safety with the benefit of less fire damage on one hand, or lower building costs for a well defined fire safety on the other hand.

#### 3. Future possibilities

New fields of application for composite structural elements can be expected in the very next future by new developments in material technology and structural analysis [7, 8].

Numerical simulations of the component interaction together with combinations of the well known basic cross-section types lead to improved shapes for beams and columns (fig. 11). Experimental results confirmed the reliability of this new design procedure. This improved cross-section design enhanced as well load bearing capacity as fire resistance.

New developments in material technology open new fields of applications for composite elements. Improved light weight concrete with no tendency towards explosive spalling, promotes the application of composite beams in light frame structures. Consequently industrial halls could be covered by a fire proof composite roof structure with visible steel surfaces and increased load bearing capacity. New high temperature resistant cements will improve the design of hollow section composite columns with unprotected steel surface, high slenderness and high fire resistance. Heat absorbing concrete for encased steel profiles and rolled profiles of the highest steel quality can be combined in order to conceive high load bearing columns for long fire resistance times.

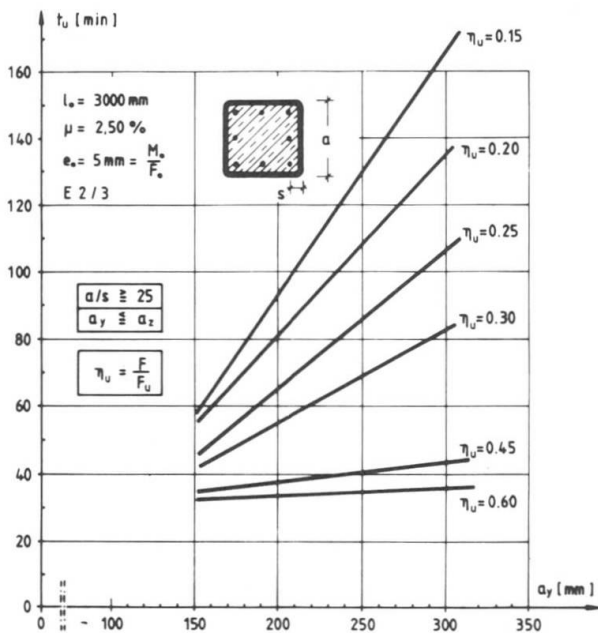


**Fig. 5** AF 90 column with gussets for beam connection: Office building TRADE ARBED, Cologne, W-Germany, 1980

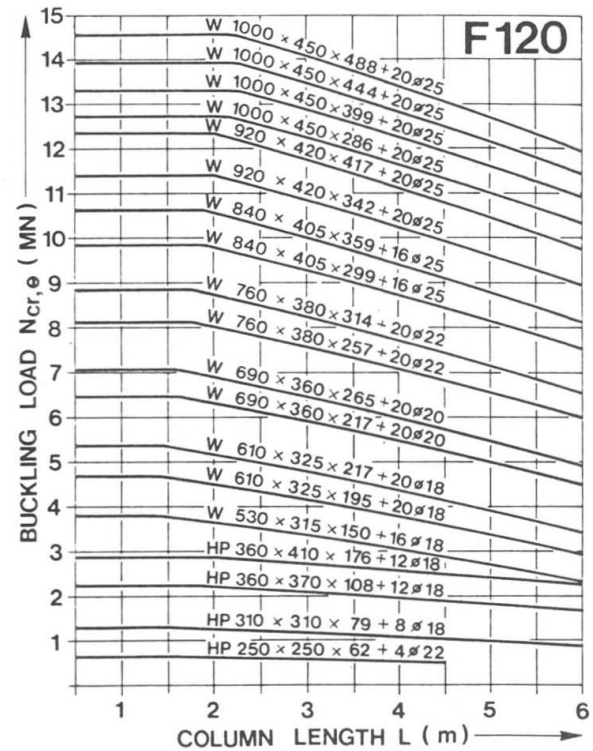


**Fig. 6** Composite columns with encased hot rolled H-profiles and steel shear heads: Office building LE FOYER, Luxembourg, 1982

**Fig. 7** Influence of load level  $\eta$  and cross section size  $a$  on failure time  $t_u$  of composite columns on concrete filled hollow sections



**Fig. 8** F 120-design diagram for AF columns, American wide flange shapes W 10''x 10'' to 40''x 18'' concreted between flanges ( $\beta_V/\beta_C = 355/45$  N/mm<sup>2</sup>)





Composite structural elements composed of rolled H-profiles either completely embedded in concrete or concreted between the flanges, could be prefabricated in a more economical way by using the adequate steel-fibre concrete technology; by this the high labour cost involving stirrup reinforcement can be dropped.

A wide application of composite construction elements in engineering, presumes the availability of good prepared design tables, graphs - not only for service load design but also for fire engineering. Such informations are already available or will be worked up in function of running research projects (fig. 12). But cross-section improvement discussed above will remain an individual analysis, which cannot be completely solved by practical design tools; for fire design the problems are similar f.i. for columns with normal force and bending moment interaction. It's a new generation of computer programmes developed for computer aided calculation and design and running on micro computers, which will support this tendency of wider application. Using these programmes, calculation and design of single construction members could be done easily by consulting engineers. Complete structures could even be analysed in order to activate the advantage of construction member interaction, so leading to a more economic design of the structural elements. Especially for fire design this is of fundamental importance (fig. 13).

The high rotative capacity of composite steel-concrete beams and columns notifies a high seismic resistance of these structural members.

Japanese investigations in this field clearly indicate wide and important applications in civil engineering. The combination of seismic resistance and fire safety in addition to the well known traditional advantages of composite steel-concrete structural elements, will activate a new trendsetting technology for buildings in seismic areas.

The above mentioned new aspects of prefabrication and material development can support this tendency.

#### B I B L I O G R A P H Y

- [1] ECCS, TC3 - Calculation of the Fire Resistance of Composite Concrete Slabs with Profiled Steel Sheet Exposed to the Standard Fire - Brussels, 1984.
- [2] JUNGBLUTH O., FEYEREISEN H., OBEREGGE O. -Verbundprofilkonstruktionen mit erhöhter Feuerwiderstandsdauer - Bauingenieur 55, 1980.
- [3] SCHLEICH J.B., LAHODA E., LICKES J.P., HUTMACHER H., - A new technology in fireproof steel construction - Acier, Stahl, Steel, 3/1983.
- [4] KLINGSCH W., K.-G. Würker, R. Martin-Bullmann,- Brandverhalten von Hohlprofil- Verbundstützen - Stahlbau, 10/1984.
- [5] KLINGSCH W., BODE H.G., FINSTERLE A. - Brandverhalten von Verbundstützen aus vollständig einbetonierten Walzprofilen - Bauingenieur 59, 1984.
- [6] SCHLEICH J.B. - Fire Safety Design of Composite Columns - International Conference "Fire Safe Steel Construction; Practical Design", Luxembourg, April 1984.
- [7] DOTREPPE J.C1., FRANSSSEN J.M., SCHLEICH J.B. - Computer Aided Fire Resistance for Steel and Composite Structures - Acier, Stahl, Steel, 3/1984.
- [8] SCHLEICH J.B. - Neuentwicklungen auf dem Gebiet des feuerwiderstandsfähigen Verbundbaus auf der Basis von Walzträgern - Fachtagung, "Stahlbau für Hochschullehrer", Köln, 21.- 23. März 1985.

$t_u$	$L_0$	PROFILE				remarks			
		HE	$d_2$	HD	$d_2$				
30	≤ 6000	≥ 100A	≥ 250	2210 .	240				
				210 . 46					
	≥ 100B	≥ 240	2260 .						
			2260 . 73						
60	≤ 6000	≥ 100A	≥ 250	2310 .	240				
				310 . 97					
	≥ 100B	≥ 240	2360 .						
			360 . 134						
90	≤ 4500	≥ 100B	≥ 250	2400 .	240				
				400 . 187					
		≥ 200B	≥ 240	2210 .					
				210 . 87					
	≤ 6000	≥ 100M	≥ 240	2260 .		240			
				260 . 101					
		≥ 200B	≥ 250	2310 .					
				310 . 130					
120	≤ 4000	≥ 120M	≥ 250	2360 .	240				
				360 . 148					
	≥ 180M	≥ 240	2400 .						
			400 . 187						
120	≤ 4000	≥ 120M	≥ 250	2210 .	240				
				210 . 100					
	≥ 180M	≥ 240	2260 .						
			260 . 149						
120	≤ 8000	≥ 120M	≥ 250	2310 .	240				
				310 . 158					
	≥ 180M	≥ 240	2360 .						
			360 . 196						
120	≤ 8000	≥ 180M	≥ 240	2400 .	240				
				400 . 187					

Fig. 9 Fire design diagram, minimum steel profiles encased in concrete without load reduction ( $L_0$  : real column length)

Fig. 10 AF 30/120 construction system composed of composite columns and beams

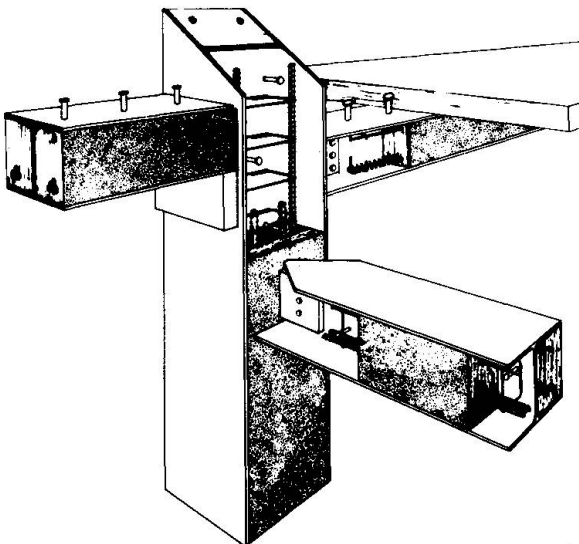
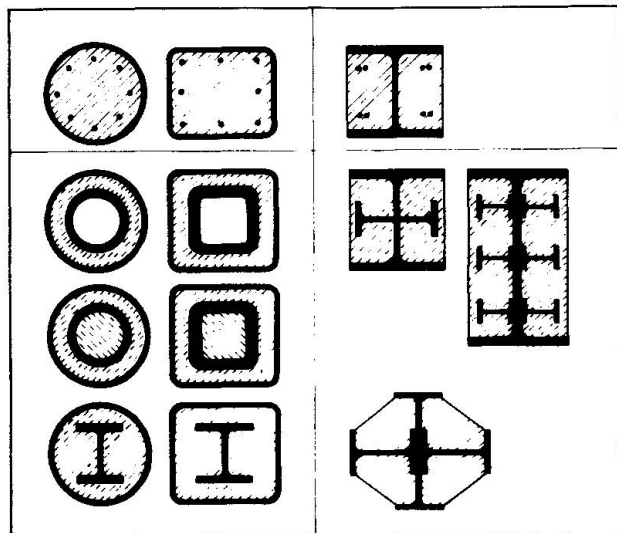


Fig. 11 Special composite cross sections





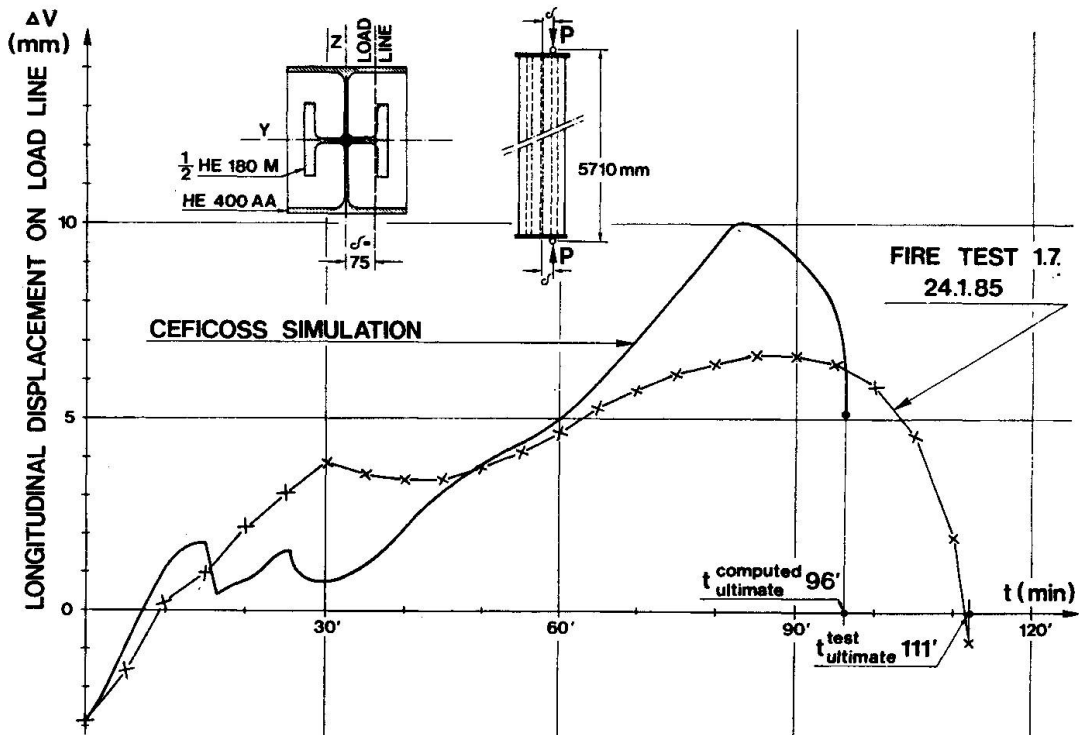


Fig. 12 Calculated [8] and measured longitudinal displacements of a composite AF column, supporting a eccentric load

Fig. 13 Different column-beam interaction possibilities in AF 30/180 construction system: pure shear connection and mixed hear-bending moment connection [8]

