

Modernisation and strengthening of large-panel building

Autor(en): **Alexandrian, Eduard**

Objektyp: **Article**

Zeitschrift: **IABSE reports = Rapports AIPC = IVBH Berichte**

Band (Jahr): **77 (1998)**

PDF erstellt am: **28.06.2024**

Persistenter Link: <https://doi.org/10.5169/seals-58236>

Nutzungsbedingungen

Die ETH-Bibliothek ist Anbieterin der digitalisierten Zeitschriften. Sie besitzt keine Urheberrechte an den Inhalten der Zeitschriften. Die Rechte liegen in der Regel bei den Herausgebern.

Die auf der Plattform e-periodica veröffentlichten Dokumente stehen für nicht-kommerzielle Zwecke in Lehre und Forschung sowie für die private Nutzung frei zur Verfügung. Einzelne Dateien oder Ausdrucke aus diesem Angebot können zusammen mit diesen Nutzungsbedingungen und den korrekten Herkunftsbezeichnungen weitergegeben werden.

Das Veröffentlichen von Bildern in Print- und Online-Publikationen ist nur mit vorheriger Genehmigung der Rechteinhaber erlaubt. Die systematische Speicherung von Teilen des elektronischen Angebots auf anderen Servern bedarf ebenfalls des schriftlichen Einverständnisses der Rechteinhaber.

Haftungsausschluss

Alle Angaben erfolgen ohne Gewähr für Vollständigkeit oder Richtigkeit. Es wird keine Haftung übernommen für Schäden durch die Verwendung von Informationen aus diesem Online-Angebot oder durch das Fehlen von Informationen. Dies gilt auch für Inhalte Dritter, die über dieses Angebot zugänglich sind.



Modernisation and Strengthening of Large-Panel Building

Eduard ALEXANDRIAN
Head of the Laboratory
TbilZNIIEP
Tbilisi, Georgia



Eduard Alexandrian, born 1919, civil and industrial engineering, candidate of technical science. For over 30 years has studied the problems of strengthening and restoration of damaged buildings.

Summary

The paper describes modernisation of a large-panel building, series 1-335 in Krasnodar. Attention is paid to the structural solution of such buildings and the design drawbacks which resulted in significant corrosion of important joints of bearing structures, overnormative deflection of floor slabs, etc. The paper presents developed, tested and introduced solutions on elimination the drawbacks of the structure. Also considered are the questions of durability and reliability of epoxy mortars in construction based on the results of long-term studies of the author and observation over the operation of the buildings restored and strengthened by epoxy mortars.

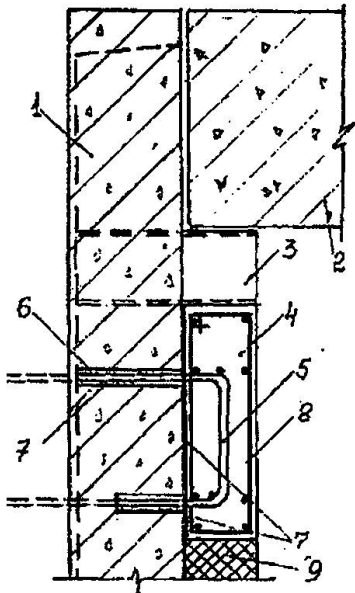
1. Modernisation of Large-Panel Buildings, Series 1-335 in Krasnodar (Russia)

In the process of building and exploitation of large-panel buildings of series 1-335, one of the mass building series of the first generation in the former Soviet Union, an urgent necessity of solving a number of architectural and structural problems arose. Besides that these houses deteriorated and required overhaul repair and modernisation. The structure of these houses consists of outside wall panels and inside frame, the main elements of which - cross-bars - are supported by the columns spaced along the middle longitudinal axis of the building and by the outside bearing wall panels. The wall panel presents a thin ribbed slab 30 mm wide with warmth-keeping jacket of non steam cured foam concrete 300 mm wide. The load from the cross-bars to the outside wall panels is transferred through the cantilevers made of channels N12 embedded in the ribs of the panels with the cross-section 175 x 150. The floor slabs, width 100 mm, are supported from both sides by cross-bars, cross-section 200 x 350 mm.

Presented below are the solutions of a number of technical problems developed by TbilZNIIEP concerning the elimination of structural drawbacks in the buildings of series 1-335. The solutions were approved in Krasnodar (Russia) in 1989 in one of the first experiments in the Soviet Union on the Modernisation of large-panel buildings of the first generation.

1.1 Strengthening of the joints "Cross-Bars Supported by Wall Panels"

Examination of the buildings of series 1-335 after 10-12 years of operation in different towns revealed corrosion of load bearing embedded details of channels N12. In Leningrad, e.g., corrosion was 0.5 mm on the average on every open surface amounting to 1 mm in some



places. Corrosion of the embedded details was mainly due to the "bridges" of cold formed in double-layer panels due to the wrongly selected warmth-keeping jacket of non steam cured foam concrete of low strength, weak adhesion with reinforced concrete panel and high hygroscopicity. Taking into account the danger of exploitation of the buildings with such joints it was suggested that reinforced concrete monolithic or prefabricated columns 200 x 200 mm, height 2.20 m should be placed under existing cantilevers on each floor and additional foundation should be arranged with the column in the sub-floor // (LenZNIIEP). This method alongside with great labour expenditures was connected with the necessity of erection of long-size column elements through window openings. TbilZNIIEP has solved this problem by gluing prefabricated reinforced concrete elements - cantilevers to the wall panel ribs - by means of polymer mortar against the stop to the existing cantilevers. Anchor free lengths of cantilevers were glued into the pits previously drilled in the ribs (fig. 1).

Fig. 1 Strengthening of the joint 'cross-bars supported by wall panels'

1 - wall panel rib; 2 - cross-bar; 3 - channel No. 12; 4 - strengthening cantilever; 5 - anchor; 6 - pit, $d = 25$ mm; 7 - polymer mortar; 8 - cantilever reinforcement, 9 - warmth-keeping jacket-foam concrete

To fix the newly built loggias to the existing wall panels from the yard facade anchors of the cantilevers were roved through the pit in the rib and welded to the embedded details of the previously arranged vertical panels of loggias. Shear tests of a full-size reinforced concrete cantilever glued to the panel rib fragment showed that the patterns were damaged mainly in tile concrete close to the glue joint and anchor rupture. The bearing capacity of the strengthening structure was 1.5 - 2 times that of the designed one determined according to /3/ as the design of an embedded detail. Hence the design of anchor cross-section area of the strengthening cantilever can be analogous to he design of anchor cross-sections of embedded details /3/.

Having found the area and the diameter of the anchor - d and assuming the diameter of polymer mortar casing - d_0 it is possible to determine the length of the anchorage of free lengths of reinforcement bars of the cantilever - l by formula

$$l \geq \frac{d^2 R_s}{4d_0 R_{b,sh} \gamma_{bi}}$$

where R_s - designed stretch resistance of the reinforcement, $R_{b,sh}$ -actual strength of concrete: panel rib shear strength assumed to be $R_{b,sh} = 1.58 R_{br}$ where R_{br} -tensile strength of concrete